## ETAP IEC Short-Circuit

This document provides an ETAP validation case. This is just one of many test case scenarios for IEC ShortCircuit (SCIEC) which are part of ETAP V\&V program. This case is a validation case based on comparisons against published results in the IEC TR 60909-4:2021 document for Short-Circuit analysis.

## Short-Circuit IEC Comparison Case \# 2

## Comparison of ETAP Short-Circuit IEC Calculations against Published Example

## Excerpt from Validation Cases and Comparison Results (TCS-SCIEC-201)

## Highlights

- Comparison of ETAP SCIEC results against published results in IEC TR 60909-4:2021 [1] Example-8 (Page 59-72).
- Comparisons for:
- Initial symmetrical current ( I "k).
- Peak current (Ip) for both method B and C.
- Breaking Current (Ib)


## System Description

Example 8 of [1] examines 3-phase fault current results for conventional and IBR (Inverter Based Resource) wind power plant combinations. The one-line diagram shown in Figure 1 was generated using the data provided in [1]. A detailed breakdown of three-phase fault results for each wind turbine technology combination is provided in Table 1. Detailed short-circuit results for each combination are provided in Tables 2 to 7.

Table 1: Summary of Wind Turbine Technology Combinations

| Case \# | Tables Listing <br> Comparisons | Scenario Description |
| :--- | :---: | :--- |
| Case 1 | Table 2 | Wind power plant consists of ten wind power station units with doubly fed asynchronous <br> generators. |
| Case 1B | Table 3 | Case 1 with cables L2 to L12 are neglected. |
| Case 2 | Table 4 | Wind power plant consists of ten wind power station units with full size converters. |
| Case 2B | Table 5 | Case 2 with cables L2 to L12 are neglected. |
| Case 3 | Table 6 | Wind power plant consists of five wind power station units with doubly fed asynchronous <br> generators (W1 to W5 in Figure 1) and five wind power station units with full size <br> converter (W6 to W10 in Figure 1). |
| Case 3B | Table 7 | Case 3 now with cables L2 to L12 are neglected. |



Figure 1: ETAP One line diagram showing the example from section 8 of IEC60909-4-2021

## Comparison of Results

Table 2 to Table 7 list comparisons between the ETAP and the results published in example 8 of [1].
The maximum deviation in the results is less than $2 \%$ for cases 2 to 3 B. WTGs with the full converters in ETAP are modeled as voltage dependent current sources and is an iterative process. The proportion of active and reactive components of the current are based on the reactive current priority option in ETAP. This option uses the fault ride through (FRT) characteristics which depend on the pre-fault loading conditions and are not provided in the example. However, if the manufacturer data for the Short-Circuit power factor is available then the percent deviation in the ETAP results would be reduced.

Table 2: Initial Symm. and Peak Currents (method B and C) for Case 1

|  | IEC | ETAP |  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault Location | $\begin{array}{r} \mathbf{I} " \mathbf{k} \\ (\mathbf{k} \mathbf{A}) \end{array}$ | $I^{\prime \prime} k$ $(\mathbf{k A})$ | $\begin{gathered} \% \\ \text { Diff. } \end{gathered}$ | $\operatorname{Ip}(\mathbf{k A})$ <br> Method B | Ip (kA) <br> Method B | \%Diff | $\underset{\text { Method C }}{\operatorname{Ip}(k A)}$ | $\begin{gathered} \text { Ip (kA) } \\ \text { Method C } \end{gathered}$ | \%Diff |
| F1 | 10.745 | 10.745 | 0.00 | 26.503 | 26.503 | 0.00 | 26.504 | 26.504 | 0.00 |
| F2 | 9.045 | 9.045 | 0.00 | 23.085 | 23.085 | 0.00 | 23.129 | 23.128 | 0.00 |
| F3 | 6.978 | 6.978 | 0.00 | 15.403 | 15.403 | 0.00 | 15.469 | 15.469 | 0.00 |
| F4 | 6.385 | 6.385 | 0.00 | 14.816 | 14.816 | 0.00 | 12.974 | 12.974 | 0.00 |
| F5 | 6.095 | 6.095 | 0.00 | 13.629 | 13.629 | 0.00 | 11.945 | 11.945 | 0.00 |
| F6 | 6.568 | 6.568 | 0.00 | 13.604 | 13.604 | 0.00 | 13.698 | 13.698 | 0.00 |
| F7 | 6.478 | 6.478 | 0.00 | 13.249 | 13.250 | 0.00 | 13.348 | 13.348 | 0.00 |
| F8 | 6.262 | 6.262 | 0.00 | 14.307 | 14.307 | 0.00 | 12.540 | 12.540 | 0.00 |
| F9 | 6.184 | 6.184 | 0.00 | 13.986 | 13.986 | 0.00 | 12.262 | 12.262 | 0.00 |
| F10 | 6.513 | 6.513 | 0.00 | 13.402 | 13.402 | 0.00 | 13.517 | 13.517 | 0.00 |
| F11 | 6.394 | 6.394 | 0.00 | 14.892 | 14.892 | 0.00 | 13.075 | 13.075 | 0.00 |
| F12 | 6.247 | 6.247 | 0.00 | 14.273 | 14.273 | 0.00 | 12.542 | 12.542 | 0.00 |
| F13 | 5.993 | 5.993 | 0.00 | 13.271 | 13.270 | 0.00 | 11.670 | 11.670 | 0.00 |
| F14 | 6.313 | 6.313 | 0.00 | 14.546 | 14.545 | 0.00 | 12.773 | 12.773 | 0.00 |

Table 3: Initial Symm. and Breaking Currents for Case 1B

|  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault Location | $\mathbf{I} \mathbf{\prime \prime} \mathbf{k}(\mathbf{k A})$ | $\mathbf{I} \mathbf{I}^{\prime \prime}(\mathbf{k A})$ | \% Diff. | $\mathbf{I b}(\mathbf{k A})$ | $\mathbf{I b}(\mathbf{k A})$ | \% Diff. |
| F1 | 10.747 | 10.747 | 0.00 | 10.679 | 10.679 | 0.00 |
| F2 | 9.056 | 9.056 | 0.00 | 8.383 | 8.383 | 0.00 |
| F3 | 6.988 | 6.988 | 0.00 | 6.083 | 6.083 | 0.00 |

Table 4: Initial Symm. and Peak Currents (method B and C) for Case 2

|  | IEC | ETAP |  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault <br> Location | I'k (kA) | I'k (kA) | \% Diff. | Ip (kA) <br> Method B | Ip(kA) <br> Method B | \% Diff. | Ip(kA) <br> Method C | Ip(kA) <br> Method C | \% Diff. |
| F1 | 10.671 | 10.642 | -0.27 | 26.168 | 26.168 | 0.00 | 26.168 | 26.168 | 0.00 |
| F2 | 8.387 | 8.222 | -1.97 | 20.785 | 20.785 | 0.00 | 20.785 | 20.785 | 0.00 |
| F3 | 6.161 | 6.075 | -1.40 | 14.183 | 14.053 | -0.92 | 12.506 | 12.377 | -1.03 |
| F4 | 5.728 | 5.677 | -0.90 | 12.341 | 12.267 | -0.60 | 10.894 | 10.820 | -0.68 |
| F5 | 5.522 | 5.482 | -0.72 | 11.583 | 11.526 | -0.49 | 10.230 | 10.173 | -0.55 |
| F6 | 5.852 | 5.775 | -1.32 | 12.817 | 12.701 | -0.91 | 11.312 | 11.198 | -1.01 |
| F7 | 5.787 | 5.711 | -1.31 | 12.304 | 12.442 | 1.12 | 11.083 | 10.971 | -1.01 |
| F8 | 5.633 | 5.585 | -0.87 | 11.977 | 11.907 | -0.58 | 10.576 | 10.506 | -0.66 |
| F9 | 5.577 | 5.531 | -0.82 | 11.773 | 11.708 | -0.55 | 10.397 | 10.332 | -0.63 |
| F10 | 5.797 | 5.723 | -1.27 | 12.580 | 12.470 | -0.88 | 11.106 | 10.997 | -0.98 |
| F11 | 5.708 | 5.654 | -0.94 | 12.230 | 12.154 | -0.62 | 10.799 | 10.724 | -0.70 |
| F12 | 5.600 | 5.552 | -0.85 | 11.829 | 11.762 | -0.57 | 10.448 | 10.381 | -0.64 |
| F13 | 5.419 | 5.378 | -0.74 | 11.199 | 11.141 | -0.51 | 9.895 | 9.838 | -0.57 |
| F14 | 5.651 | 5.600 | -0.89 | 12.018 | 11.947 | -0.59 | 10.614 | 10.542 | -0.68 |

Table 5: Initial Symm. and Breaking Currents for Case 2B

|  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault Location | I'k (kA) | $\mathbf{I} \mathbf{\prime \prime k}(\mathbf{k A})$ | \% Diff. | Ib (kA) | Ib (kA) | \% Diff. |
| F1 | 10.671 | 10.642 | -0.27 | 10.671 | 10.642 | -0.27 |
| F2 | 8.387 | 8.222 | -1.97 | 8.387 | 8.222 | -1.97 |
| F3 | 6.161 | 6.075 | -1.40 | 6.161 | 6.075 | -1.40 |

Table 6: Initial Symm. and Peak Currents (method B and C) for Case 3

|  | IEC | ETAP |  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault <br> Location | I"k <br> (kA) | I'k <br> (kA) | \% Diff. | Ip(kA) <br> Method B | Ip (kA) <br> Method B | \%Diff | Ip(kA) <br> Method C | Ip (kA) <br> Method C | \%(Diff |
| F1 | 10.713 | 10.695 | -0.17 | 30.197 | 30.171 | -0.09 | 26.365 | 26.339 | -0.10 |
| F2 | 8.734 | 8.646 | -1.01 | 24.072 | 23.945 | -0.53 | 22.075 | 21.948 | -0.58 |
| F3 | 6.570 | 6.519 | -0.77 | 15.948 | 15.874 | -0.46 | 13.992 | 13.919 | -0.52 |
| F4 | 6.078 | 6.059 | -0.30 | 12.008 | 11.981 | -0.22 | 12.073 | 12.047 | -0.22 |
| F5 | 5.834 | 5.822 | -0.21 | 12.762 | 12.744 | -0.14 | 11.244 | 11.226 | -0.16 |
| F6 | 6.232 | 6.183 | -0.79 | 14.379 | 14.308 | -0.50 | 12.654 | 12.583 | -0.56 |
| F7 | 6.157 | 6.137 | -0.32 | 12.307 | 12.278 | -0.23 | 12.380 | 12.351 | -0.24 |
| F8 | 5.976 | 5.961 | -0.25 | 11.659 | 11.637 | -0.19 | 11.734 | 11.712 | -0.18 |
| F9 | 5.910 | 5.896 | -0.23 | 13.059 | 13.039 | -0.15 | 11.510 | 11.490 | -0.18 |
| F10 | 6.124 | 6.091 | -0.54 | 13.796 | 13.749 | -0.34 | 12.115 | 12.067 | -0.39 |
| F11 | 6.015 | 5.985 | -0.51 | 13.339 | 13.296 | -0.33 | 11.715 | 11.672 | -0.37 |
| F12 | 5.884 | 5.856 | -0.48 | 12.823 | 12.783 | -0.32 | 11.264 | 11.223 | -0.36 |
| F13 | 5.666 | 5.643 | -0.40 | 12.024 | 11.991 | -0.27 | 10.563 | 10.531 | -0.31 |
| F14 | 5.946 | 5.916 | -0.50 | 13.066 | 13.023 | -0.33 | 11.476 | 11.433 | -0.37 |

Table 7: Initial Symm. and Breaking Currents for Case 3B

|  | IEC | ETAP |  | IEC | ETAP |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fault <br> Location | $\mathbf{I ' k}(\mathbf{k A})$ | $\mathbf{I ' k}(\mathbf{k A})$ | \% Diff. | Ib (kA) | Ib (kA) | \% Diff. |
| F1 | 10.714 | 10.695 | -0.18 | 10.661 | 10.650 | -0.10 |
| F2 | 8.739 | 8.651 | -1.01 | 8.348 | 8.292 | -0.67 |
| F3 | 6.574 | 6.523 | -0.77 | 6.122 | 6.111 | -0.19 |

## References

[1] IEC TR 60909-4:2021, Short-circuit currents in three-phase AC systems -Part 4: Examples for the calculation of short-circuit currents, Geneva, Switzerland: IEC
[2] ETAP Short Circuit IEC V\&V Documents, Case Number TCS-SCIEC-201.

